

On the mesh relaxation time in the moving mesh method

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Outline

- Background: MMPDE's
- Motivation: Self-similar blow-up
- Numerical simulations
- Future work

Background: Moving mesh PDE's

Moving mesh method

- $x =$ physical coordinate, $\xi =$ computational coordinate
- One-to-one mapping: $x(\xi, t)$, $\xi \in [0, 1]$
- Monitor function: $M(x, t) > 0$
- Equidistribution Principle (EP, integral form):

$$\int_0^{x(\xi, t)} M(x', t) dx' = \xi \theta(t) \quad \text{where} \quad \theta(t) = \int_0^1 M(x', t) dx'$$

- Equidistribution Principle (EP, differential form):

$$\frac{\partial}{\partial \xi} \left(M \frac{\partial x}{\partial \xi} \right) = 0$$

Moving mesh PDE's

Huang, Ren & Russell (1994):

- Equidistribution Principle

$$\frac{\partial}{\partial \xi} \left[M(x(\xi, t), t) \frac{\partial}{\partial \xi} x(\xi, t) \right] = 0$$

Moving mesh PDE's

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- Introduce a **relaxation time τ**

$$\frac{\partial}{\partial \xi} \left[M(x(\xi, t + \tau), t + \tau) \frac{\partial}{\partial \xi} x(\xi, t + \tau) \right] = 0$$

Moving mesh PDE's

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- Introduce a **relaxation time** τ

$$\frac{\partial}{\partial \xi} \left[M(x(\xi, t + \tau), t + \tau) \frac{\partial}{\partial \xi} x(\xi, t + \tau) \right] = 0$$

- Expand in Taylor series:

$$\text{(MMPDE4)} \quad \frac{\partial}{\partial \xi} \left(M \frac{\partial x}{\partial \xi} \right) = - \frac{1}{\tau} \frac{\partial}{\partial \xi} \left(M \frac{\partial x}{\partial \xi} \right)$$

$$\text{(MMPDE6)} \quad \frac{\partial^2 x}{\partial \xi^2} = - \frac{1}{\tau} \frac{\partial}{\partial \xi} \left(M \frac{\partial x}{\partial \xi} \right)$$

Mesh relaxation time

- While a large effort has been expended on developing better monitor functions, almost no attention has been paid to the choice of τ
- τ is identified as an important parameter **BUT** it's
 - ◆ always taken to be constant
 - ◆ tuned by trial-and-error for a given problem
- τ can be interpreted in several ways:
 - ◆ a relaxation time for the mesh to satisfy the EP
 - ◆ temporal smoothing
 - ◆ a damping factor – **Adjerid & Flaherty (1986)**
 - ◆ a delay factor – **Furzeland et al. (1990)**

Mesh relaxation time (2)

In practice, the choice of τ is a trade-off:

- τ must be large enough to avoid oscillations in the mesh (stability)
- τ must be small enough that mesh can respond to changes in the solution (accuracy)

| | <i>accuracy</i> | <i>stiffness / cost</i> |
|--------------------------------|-----------------|--------------------------|
| <i>small τ</i> | increased | more stiff / higher cost |
| <i>large τ</i> | decreased | less stiff / lower cost |

Basic idea

- For problems with complex behaviour (esp. time variations on fast and slow scales) choosing a single constant value of τ seems inappropriate

- Instead, we want

mesh time scale \approx solution time scale

- Examples:

- a. *blow-up*: initial rapid motion of mesh points – **Budd, Huang & Russell (1996)**
- b. *moving fronts*: with variable front speed – **JS, Mackenzie & Russell (2001)**
- c. *Gierer-Meinhardt*: very slow spike motion, with rapid, spontaneous changes – **Iron & Ward (2002)**

Aim: Increase accuracy and efficiency by varying $\tau(t)$ throughout a computation

Blow-up problems

A simple blow-up model

- One of the simplest models for blow-up is (for $p > 1$)

$$u_t = u_{xx} + u^p \quad \text{subject to} \quad \begin{aligned} u(0, t) = u(1, t) &= 0 \\ u(x, 0) &= u_0(x) \end{aligned}$$

- The solution “blows up” at $x = x^*$ and $t = t^*$ if:

$$\begin{aligned} u(x^*, t) &\rightarrow \infty \quad \text{as } t \rightarrow t^* \\ \text{and } u(x, t) &\rightarrow u(x, t^*) < \infty \quad \text{if } x \neq x^* \end{aligned}$$

- There is a similarity solution with asymptotic behaviour

$$u(x, t) \longrightarrow \beta^\beta (t^* - t)^{-\beta} \left(1 + \frac{\mu^2}{4p\beta} \right)^{-\beta} \quad \text{as } t \rightarrow t^*$$

where $\beta = \frac{1}{p-1}$ and μ is the *ignition kernel*

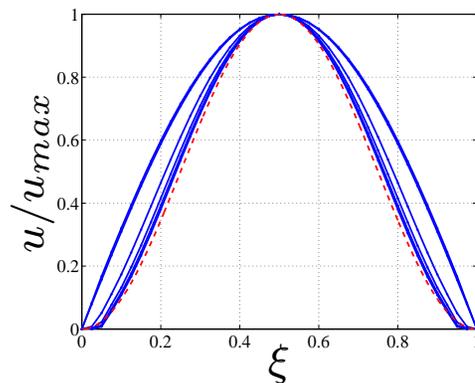
– **Bebernes & Bricher (1992)**

Moving mesh calculations of blow-up

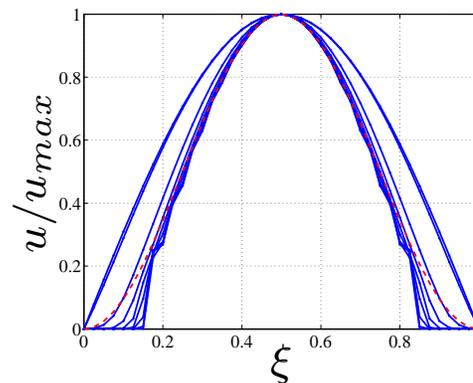
Budd, Huang & Russell (1996):

- Used the MMPDE approach to compute self-similar solutions (fixed mesh calculations are pointless!)
- Derived the monitor $M = u^{p-1}$ needed to capture self-similarity
- With $p = 2$ and $N = 40$ points:

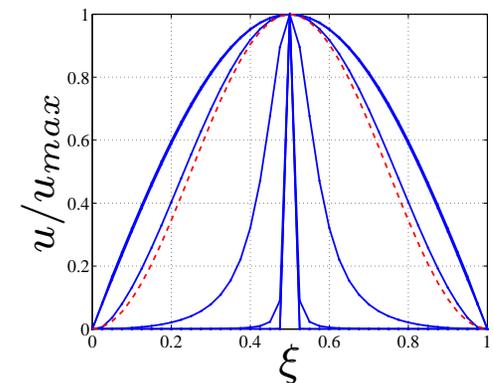
MMPDE6, $\tau = 10^{-5}$



MMPDE6, $\tau = 10^{-1}$

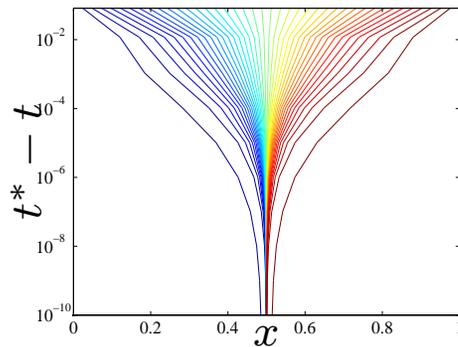


MMPDE4, $\tau = 10^{-5}$

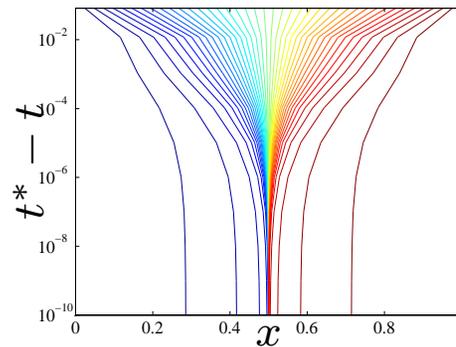


Moving mesh calculations of blow-up (2)

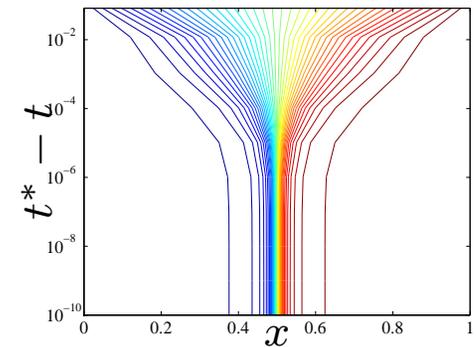
MMPDE6, $\tau = 10^{-5}$



MMPDE6, $\tau = 10^{-1}$



MMPDE4, $\tau = 10^{-5}$



Provided τ is taken small enough (e.g., $\tau = 10^{-5}$):

- both the computed solution and mesh capture self-similarity
- blow-up behaviour can be computed accurately

Choice of τ

Some insight is afforded by a scaling argument in BHR'96:

- The solution and monitor satisfy:

$$u \sim (t^* - t)^\beta \quad \text{and} \quad M = u^{p-1} \sim (t^* - t)$$

- The mesh has a natural timescale:

$$T_{mesh} = O(\tau) \quad (\text{for MMPDE4})$$

$$T_{mesh} = O\left(\frac{\tau}{M}\right) \sim \tau(t^* - t) \quad (\text{for MMPDE6})$$

- **Conclude:** MMPDE6 with $\tau = 10^{-5}$ (constant) allows the mesh to evolve even for t close to t^* , but MMPDE4 does not

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Our claim: τ need not always be so small (i.e., the mesh equation is unnecessarily stiff). A more sensible choice is:

$$\tau = \tau_o \max_x M \quad \text{with } \tau_o \ll 1$$

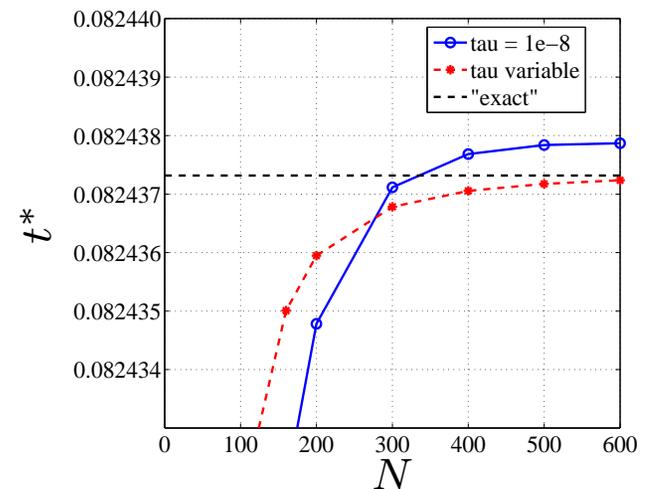
Numerical simulations

Variable τ results

- Take $p = 2$, MMPDE6, MOL + DASSL
- $\tau(t) = \tau_o \max_x M$, force $\tau \in [10^{-8}, 10^{-1}]$
- Compare to simulation with constant $\tau = 10^{-8}$

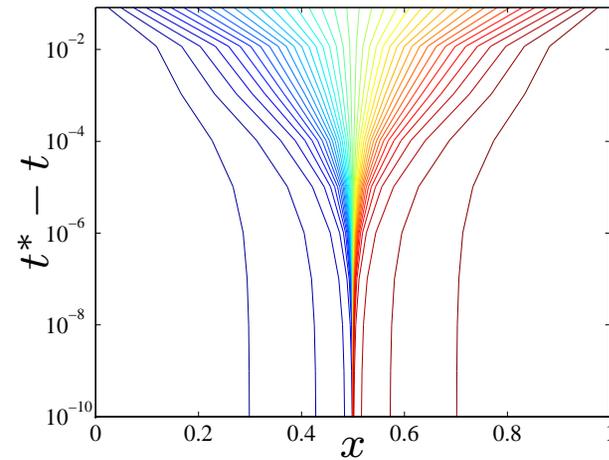
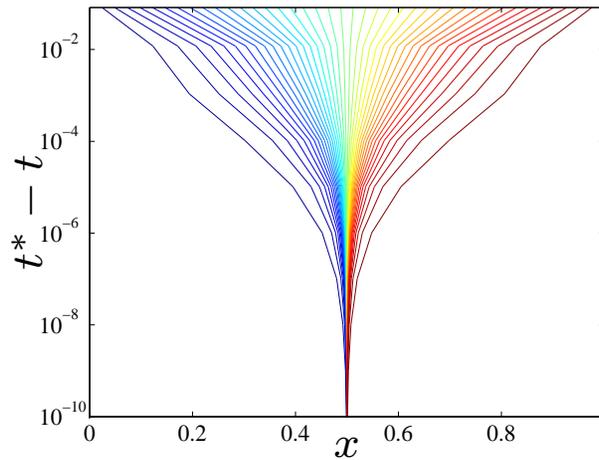
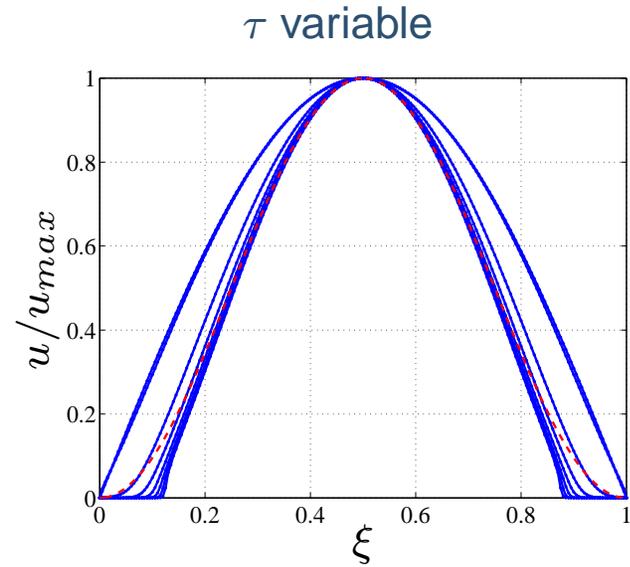
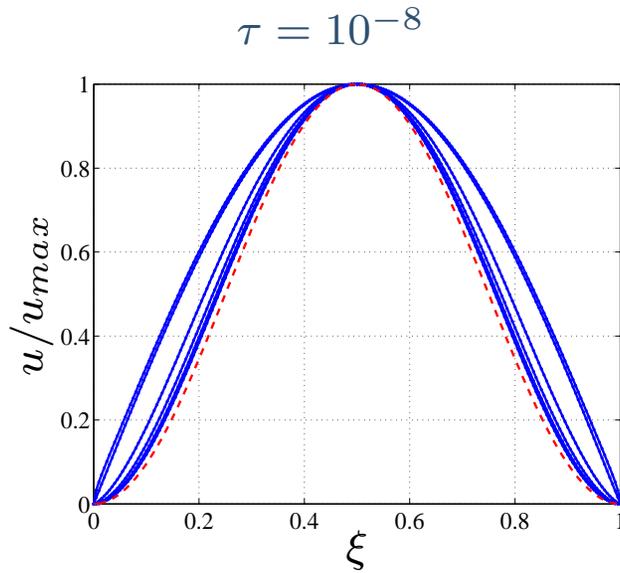
Variable τ results demonstrate:

- CPU time is reduced by at least a factor of three
- $\max_x u$ is at least 3 orders of magnitude larger (computes further into blow-up)
- t^* is computed more accurately



Variable τ results (2)

With $N = 200$ points:

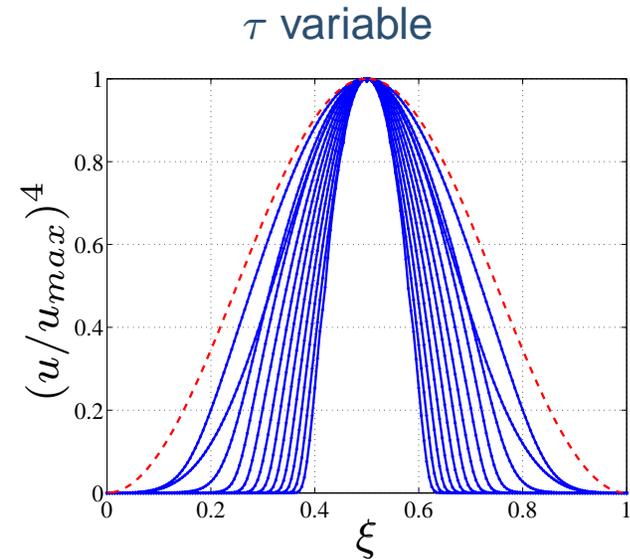
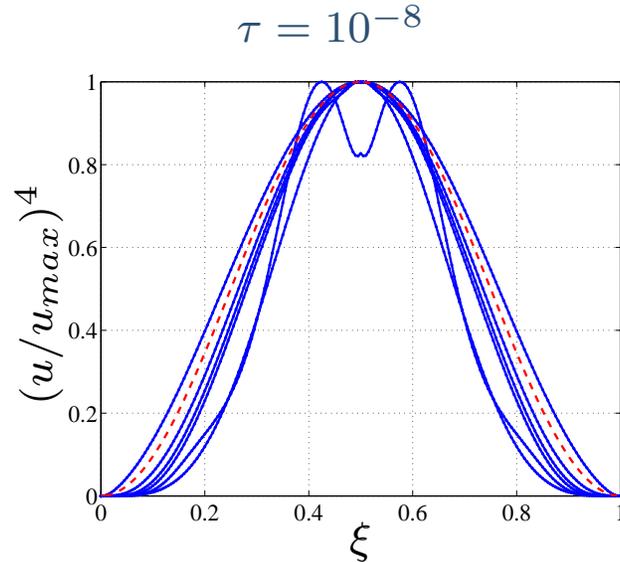


Variable τ results (3)

Summary of results:

- τ needs to be small only during the time leading up to blow-up, as mesh points race into the peak
- For t closer to t^* , it's sufficient to take $\tau = \tau_{max} = 0.1$
- Variable τ improves both accuracy and efficiency, but leads to a slight loss of self-similarity

More severe blow-up ($p = 5$)



- Non-physical oscillations appear in constant τ results, but not with variable τ
- Similar improvement in efficiency
- Variable τ results show a more significant deviation from self-similarity

Conclusions

- Choosing mesh relaxation parameter τ constant is not optimal
- Significant improvements in accuracy and cost can be obtained by varying τ sensibly for blow-up problems
- We need another approach for calculating τ adaptively in general situations

Future work

- Determine a more general form of $\tau(t)$ which is robust and applicable to other problems
 - see **Hyman & Larrouturou (1989)**, **W. Huang (2001)**
- More extensive studies involving other PDE's
- Analytical investigation, going back to the EP

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